Expedient Design Of Overhead Anchorage Systems

Assumptions

The following design sequence has been prepared as a reference for the design of overhead anchorage systems. (See figure on page 182.) Several assumptions have been made which simplify the standard design procedures. If these assumptions do not apply to a particular situation, or if an increased understanding of the design sequence is desired, refer to Chapter 8.

- All calculations are based upon the use of IPS cables.
- Deadmen will be constructed using logs or timbers.
- Flat bearing plates will be used on all deadmen.
- The depth of the ground water table at the bridge site is greate than 4 feet.
- Tidal variations or shore conditions do not require that the anchorage towers be placed a significant distance (over 75 feet) from the waterline.
- Standard Class 60 towers will be used to support the overhead cable.
- The designer is able to roughly estimate the tower to deadman slope ratio. See Chapter 8 for further guidance.

Design Data
The following information must be calculated or determined when
designing an overhead cable system:
Cable data
Number of master cables
Size of master cable(s) (CD)
Length of the master cable(s) (CL)
Size of master cable(s) (CD) Length of the master cable(s) (CL) Number of clips at each end of the cable
Spacing of cable clips
Initial sag (S)
Tower data
Actual tower height (H
Near shore
Far shore
Tower waterline distance (A)
Near shore
Far shore Tower bridge offset (O1)
Tower-bridge offset (O1)
Near shore
Far shore
Tui bhore
Deadman data
Depth of deadman (DD)
Near shore
Far shore
Tower-deadman distance (C)
Near shore
Far shore

Towerd-deadman offset (O2)	
Near shore	
Far shore	
Deadman face (Df)	
Deadman thickness (Dt)	
Deadman length (DL)	
Near shore	
Far shore	
Bearing plate thickness (x)	
Bearing plate length (y)	
Bearing plate face (z)	
Overhead Cable Design Sequence	

Step 1. Determine the size and number of master cables required. Refer to Table 57 for M4T6, Class 60, and ribbon bridge. Refer to Table 58 for light tactical bridges.

Step 2. Determine the distance between towers (1) in feet.

L = (1.1x G) + 100 feet

Where G = the width of the wet gap in feet. **Step 3.** Determine the length of the master cable (CL) in feet.

 $C_L = L + 250$ feet

Where L = the distance between towers in feet.

CL =

Note. This is an approximation based upon the most extreme circumstances.

Step 4. Determine the number of cable clips required to secure one end of the master cable.

Number of clips = (3x CD) + 1

Where CD = the cable diameter in inches

Number of clips at each end =

Step 5. Determine the spacing of cable clips in inches.

Clip spacing = (6x CD)Where CD = the cable diameter in inches

Clip spacing =

Step 6. Determine initial sag (S) in feet.

S = (.02x L)

Where L = the distance between towers in feet

Step 7. Determine tower height (H) in feet.

 \vec{a} . HR = 3 feet + S-BH

Where HR = the required tower height in feet

S = initial sag in feet BH = bank height in feet **Note.** This calculation must be done for both the near and far shore

since bank heights may be different.

b. Determine actual tower height (H). Refer to Table 59 which provides a list of possible tower heights. Compare the required tower height to the possible tower height. Select the smallest possible tower that is greater than or equal to the required height.

Note. If the near and far shore towers are determined to have different

heights, steps 8 through 16 must be calculated separately for both near

and far shores.

H near shore =

H far shore =

Step 8. Determine the distance from each tower to the waterline (A) in feet.

$$A = \frac{L - G}{2}$$

Where L = the distance between towers in feet

G = the gap width in feet

A near shore =

A far shore =

Step 9. Determine the offset from each tower to the bridge's centerline (0₁) in feet.

a. If the bank height (BH) is less than or equal to 15 feet,

then 01 = H + 50 feet

b. If the bank height (BH) is greater than 15 feet, then $0_1 = H + BH + 35$ feet

Where H = the actual tower height in feet

BH = the bank height in feet

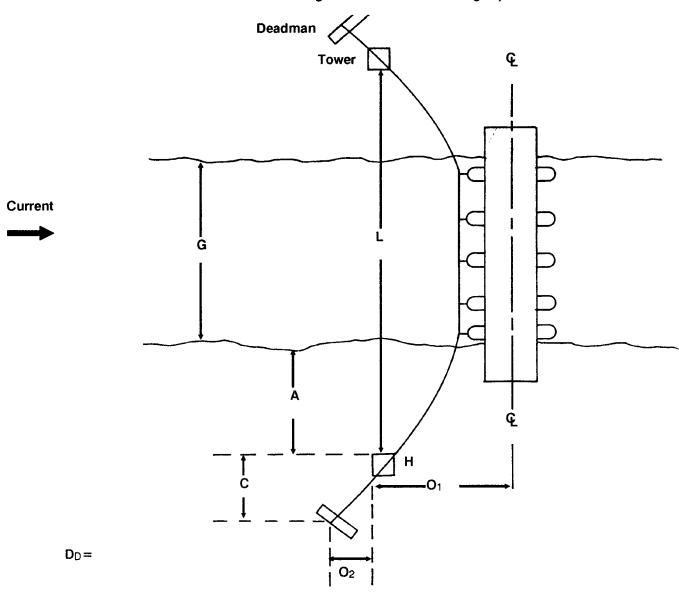
01 near shore =

01 far shore =

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Step 10. Identify deadman dimensions. Select a deadman from the
  available timbers and logs. Generally, the timber with the largest timber face/log diameter is selected. The largest timber face of that deadman is
  defined as Dithe deadman face. The thickness of that deadman is
  defined as Dt the deadman thickness.
  Df =
  Dt =
Step 11. Determine mean depth of deadman (DD) in feet.
a. There must be a minimum of 1 foot of undisturbed soil between the
  bottom of the deadman and the ground water level (GWL). Therefore
  the deepest the deadman can go (DDmax) is calculated as:
  DDmax = GWL - 1 foot - \frac{Df}{2}
  where D_f = the deadman face in feet
  GWL = depth of ground water level in feet
  b. The minimum deadman depth is always 3 feet.
  c. The maximum deadman depth is always 7 feet.
  d. Compare Domax to these minimum and maximum values to
  determine the actual mean depth of deadman (DD).
  DD near shore =
  DD far shore =
Step 12. Determine length of deadman (DL) in feet.
  \hat{D}_L = \int CC
                          + 1
         HP x Df
  Where CC = the capacity of the anchorage cable in pounds/1,000
  from Table 60.
  HP = required holding power in pounds/1,000 square feet
  from Table 61.
  Df = Deadman face in feet (for log deadman use log diameter (d))
  DL near shore =
  DL far shore =
 Step 13. Check minimum thickness of deadman (Dt) in feet.
For timber: <u>DL</u> must be less than or equal to 9
For logs: <u>DL</u> must be less than or equal to 5.
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Step 14. Determine the tower to deadman distance (C) in feet.
  C = H + DD
          slope
  Where H = the actual tower height in feet
  DD = the mean depth of deadman in feet
  slope = the tower to deadman slope
  C near shore =
  C far shore =
Step 15. Determine the tower to deadman offset (O<sub>2</sub>) in feet.
  02 = (C \times 02 \text{ feet})
  Where C = the tower to deadman distance in feet
  02 feet = a factor determined from Table 62
  0_2 near shore =
  0_2 far shore =
Step 16. Design a bearing plate for each deadman. Given deadman face
   (D<sub>f</sub>) or log diameter (d) and the size of the master cable (C<sub>D</sub>), refer to
  Table 63 to determine the length, thickness, and face of the deadman
  bearing plate.
  \mathbf{x} =
  y=
  z =
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Design of an overhead anchorage system



Appendix C 178

Table 57. Determination of cable size and number of cables for M4T6, Class 60, and ribbon bridges

Wet gap width (G)	Type bridge	Size (inches) and number of cables for specified river velocities											
(feet)	assembly		5 FPS			7 FPS		9 FPS			11 FPS		
		Single	Dual	Triple	Single	Dual	Triple	Single	Dual	Triple	Single	Dual	Triple
200	Normal	1/2	3/8	3/8	5/8	1/2	1/2	3/4	5/8	1/2	7/8	3/4	5/8
	Reinforced	5/8	1/2	3/8	3/4	5/8	1/2	7/8	3/4	5/8	1– 1/8	7/8	3/4
400	Normal	5/8	1/2	1/2	3/4	5/8	1/2	1	7/8	5/8	1-1/4	1	3/4
	Reinforced	3/4	5/8	1/2	1	3/4	5/8	1–1/4	1	3/4	1-1/2	1-1/4	7/8
600	Normai	3/4	5/8	1/2	1	3/4	5/8	1–1/4	1	3/4	1-1/2	1-1/4	7/8
	Reinforced	1	3/4	5/8	1-1/8	1	3/4	1–1/2	1-1/4	7/8	*	1-1/2	1-1/8
800	Normal	7/8	3/4	5/8	1-1/8	7/8	3/4	1-3/8	1-1/8	7/8	*	1-1/2	1-1/8
	Reinforced	1–1/8	7/8	3/4	1–3/8	1-1/8	7/8	*	1–3/8	1	*	*	1-1/4
1000	Normal	1	7/8	3/4	1-1/4	1	7/8	1–1/2	1–3/8	1	*	*	1-1/4
	Reinforced	1-1/4	1	3/4	1-1/2	1-1/4	1	*	*	1-1/8	*	*	1-3/4
1200	Normal	1–1/8	7/8	3/4	1–3/8	1–1/8	7/8	*	1-1/2	1–1/8	*	*	1–3/8
	Reinforced	1-3/8	1-3/8	7/8	*	1-3/8	1	*	*	1-1/4	*	*	*

Table 58. Determination of cable size for light tactical bridges

5 FPS	7 FPS	9 FPS	11 FPS
3/8"	3/8"	1/2"	1/2"
3/8"	1/2"	5/8"	3/4"
1/2"	1/2"	5/8"	3/4"
1/2"	5/8"	5/8"	3/4"
5/8"	5/8"	3/4"	7/8"
	3/8" 3/8" 1/2" 1/2"	5 FPS 7 FPS 3/8" 3/8" 1/2" 1/2" 1/2" 5/8"	3/8" 3/8" 1/2" 3/8" 1/2" 5/8" 1/2" 5/8" 1/2" 5/8" 5/8" 5/8"

Table 59. Possible tower heights

Tower height (H)	
3 ft 8 1/4 in	
14 ft 6 1/4 in	
25 ft 4 1/4 in	
36 ft 2 1/4 in	
47 ft 1/4 in	
57 ft 10 1/4 in	
68 ft 8 1/4 in	
	3 ft 8 1/4 in 14 ft 6 1/4 in 25 ft 4 1/4 in 36 ft 2 1/4 in 47 ft 1/4 in 57 ft 10 1/4 in

Table 60. Determination of anchorage cable in pounds/1,000

Type of cable		Cable size (in inches) (CD)										
	3/8 "	1/2 "	5/8 "	3/4 "	7/8 "	1 "	1–1/8 "	1–1/4 "	1–3/8 "	1–1/2 "		
IPS	12.6	21.6	33.2	47.4	64.4	84.0	106.0	130.0	157.0	185.0		
PS	11.0	18.8	28.8	41.2	56.0	73.0	92.0	113.0	136.0	161.0		
MPS	10.0	17.0	26.2	37.4	50.8	66.0	83.0	102.0	123.0	145.0		
	<u> </u>											

Table 61. Determination of required holding power in pounds/1,000 square feet

Depth of		Tower to de	adman slope	
deadman (D _D)	1:1	1:2	1:3	1:4
3 ft	.95	1.3	1.45	1.5
4 ft	1.75	2.2	2.6	2.7
5 ft	2.8	3.6	4.0	4.1
6 ft	3.8	5.1	5.8	6.0
7 ft	5.1	7.0	8.0	8.4

Table 62. Determination of O2 feet

Type of assembly		Cu	rrent velo	city	
	3 FPS	5 FPS	7 FPS	9 FPS	11 FPS
Normal	.09	.11	.14	.17	.19
Reinforced	.11	.14	.17	.19	.23

Table 63. Determination of bearing plate dimensions x, y, and z (in inches)

Dead	lman face (D _f)				Cable :	size (C _D)				
		3/8"	1/2"	5/8"	3/4"	7/8"	1"	1–1/8"	1-1/4"	1-1/2"
8"	X Y Z	7/16" 4" 6"	7/8" 8" 6"	1–1/4" 11" 6"						
10"	X Y Z	7/16" 4" 8"	11/16" 6" 8"	1" 9" 8"	1–3/8" 12" 8"	·				
12"	X Y Z	7/16" 4" 10"	9/16" 5" 10"	13/16" 7" 10"	1–1/8" 10" 10"	1–7/16" 13" 10"			·	
14"	X Y Z	7/16" 4" 12"	7/16" 4" 14"	11/16" 6" 12"	7/8" 8" 12"	1–1/4" 11" 12"	1–9/16" 14" 12"	2" 18" 12"		
16"	x y z	7/16" 4" 14"	7/16" 4" 14"	9/16" 5" 14"	13/16" 7" 14"	1–1/8" 10" 14"	1–3/8" 12" 14"	1–11/16" 15" 14"	2–1/8" 19" 14"	
18"	X Y Z	7/16" 4" 16"	7/16" 4" 16"	7/16" 4" 16"	11/16" 6" 16"	7/8" 8" 16"	1–1/4" 11" 16"	1–9/16" 14" 16"	1–13/16" 16" 16"	
20"	X Y Z	7/16" 4" 18"	7/16" 4" 18"	7/16" 4" 18"	11/16" 6" 18"	7/8" 8" 18"	1–1/8" 10" 18"	1–3/8" 12" 18"	1–11/16" 15" 18"	
24"	X Y Z	7/16" 4" 22"	7/16" 4" 22"	7/16" 4" 22"	9/16" 5" 22"	11/16" 6" 22"	7/8" 8" 22"	1–1/8" 10" 22"	1-3/8" 12" 22"	1–7/8" 17" 22"
	X		1 2 Y		T u v		roved Plo ng plate th ng plate le	ugh Steel nickness ength	sed upon t (IPS) cabl	